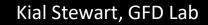
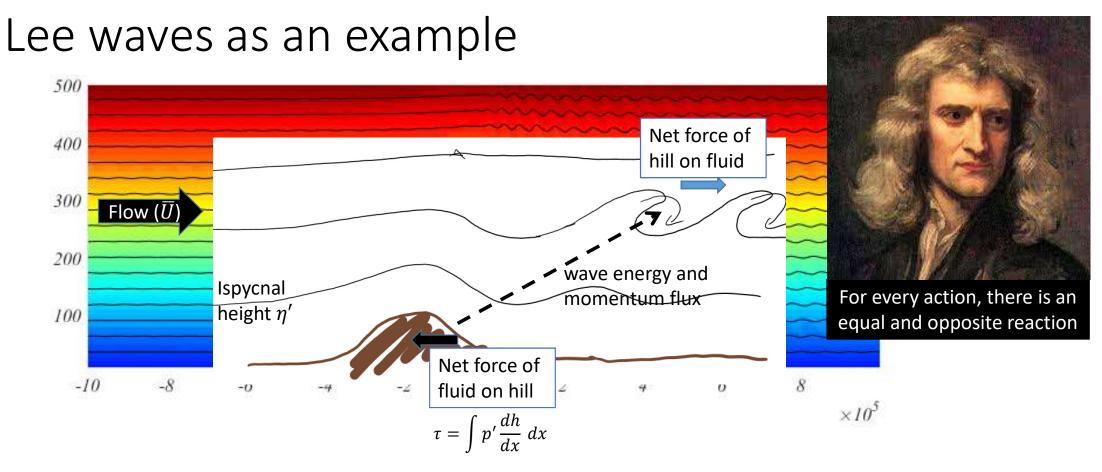
## Lecture 10: Wave-driven circulation

Callum J. Shakespeare

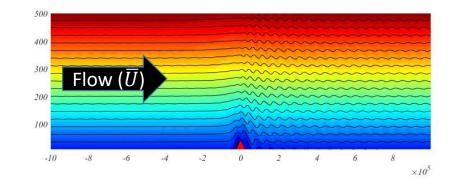
Fellow, Climate and Fluid Physics, ANU





- A NET reaction force is only felt in the layer where the wave decays/attenuates
- This could be a LONG way from the action force (hill) = "action at a distance"
- The wave transports energy and momentum between the hill and site of dissipation via form stresses  $\int p' \frac{d\eta'}{dx} dx$
- The force is given by the decay of the form stress:  $F = \frac{d}{dz} \int p' \frac{d\eta'}{dx} dx$

- Linearise z-coordinate equations about mean flow  $\overline{U}$  and stratification  $\frac{\partial b}{\partial z} = N^2$
- Assume no variation in y (ridge)
- Horizontal viscosity only = diffusivity



$$\begin{pmatrix} \frac{\partial}{\partial t} + \overline{U} \frac{\partial}{\partial x} \end{pmatrix} u - fv = -\frac{1}{\rho_0} \frac{\partial p}{\partial x} + v \frac{\partial^2 u}{\partial x^2}$$

$$\begin{pmatrix} \frac{\partial}{\partial t} + \overline{U} \frac{\partial}{\partial x} \end{pmatrix} v + fu = v \frac{\partial^2 v}{\partial x^2}$$

$$b = \frac{1}{\rho_0} \frac{\partial p}{\partial z}$$

$$\frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} = 0$$

$$\begin{pmatrix} \frac{\partial}{\partial t} + \overline{U} \frac{\partial}{\partial x} \end{pmatrix} b + N^2 w = v \frac{\partial^2 b}{\partial x^2}$$

$$Du - fv = -\frac{1}{\rho_0} \frac{\partial p}{\partial x}$$

$$Dv + fu = 0$$

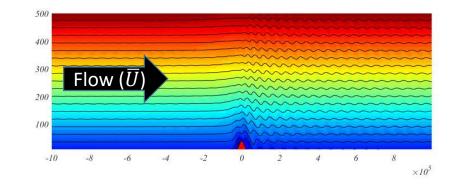
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$$Db + N^2 w = 0$$

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$$Du - fv = -\frac{1}{\rho_0} \frac{\partial p}{\partial x}$$

$$Dv + fu = 0$$

$$b = \frac{1}{\rho_0} \frac{\partial p}{\partial z}$$

$$\frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} = 0$$

$$Db + N^2 w = 0$$

$$D^2u - fDv = -D\frac{1}{\rho_0} \frac{\partial p}{\partial x}$$

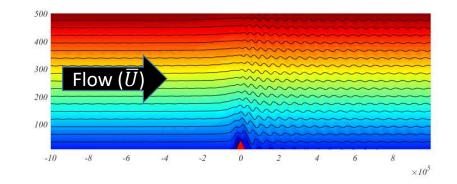
$$D^2u + f^2u = -D\frac{1}{\rho_0} \frac{\partial p}{\partial x}$$

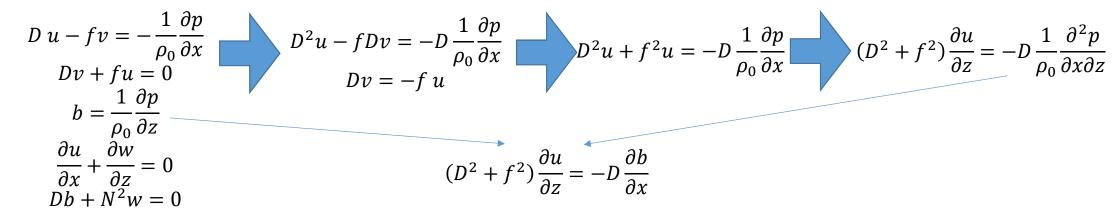
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$$D = \left(\frac{\partial}{\partial t} + \overline{U}\frac{\partial}{\partial x} - \nu\frac{\partial^2}{\partial x^2}\right)$$

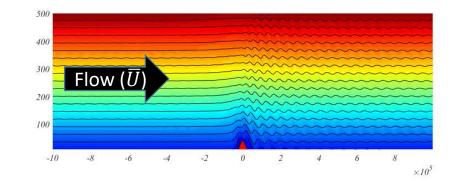
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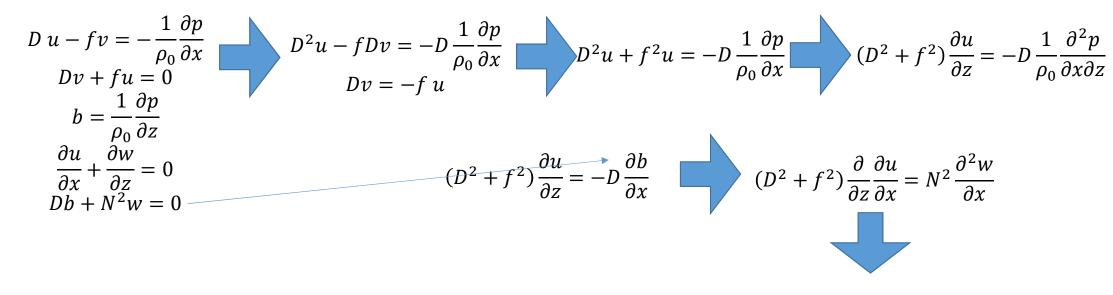




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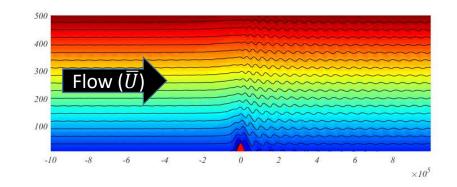
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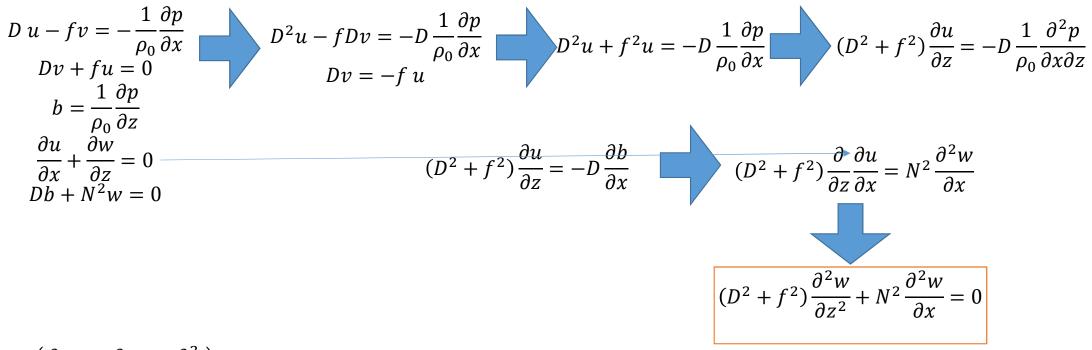




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- Linearise z-coordinate equations about mean flow  $\overline{U}$  and stratification  $\frac{\partial b}{\partial z} = N^2$
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Internal waves in a continously stratified flow

$$D = \left(\frac{\partial}{\partial t} + \overline{U}\frac{\partial}{\partial x} - \nu\frac{\partial^2}{\partial x^2}\right)$$

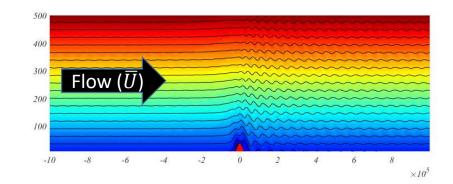
#### **Dispersion relation**

- Linearise z-coordinate equations about mean flow  $\overline{U}$  and stratification  $\frac{\partial b}{\partial z} = N^2$
- Assume no variation in y (ridge)
- Horizontal viscosity only = diffusivity

$$(D^{2} + f^{2})\frac{\partial^{2}w}{\partial z^{2}} + N^{2}\frac{\partial^{2}w}{\partial x} = 0 \qquad D = \left(\frac{\partial}{\partial t} + \overline{U}\frac{\partial}{\partial x} - \nu\frac{\partial^{2}}{\partial x^{2}}\right)$$

Let 
$$w = \widehat{w} e^{i(kx+z-\omega t)}$$
  
 $-m^2 \left( (-i\omega + ik\overline{U} + \nu k^2)^2 + f^2 \right) - k^2 N^2 = 0$ 

$$\omega = k\overline{U} \pm \sqrt{f^2 + \frac{k^2 N^2}{m^2} - i\nu k^2}$$
 What is the effect of this?



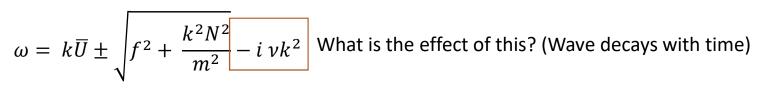
Recall: Internal wave dispersion relation for 2-layered model  $\omega = k\overline{U} \pm \sqrt{f^2 + k^2 g' h_1}$ 

#### **Dispersion relation**

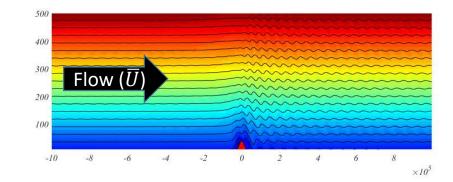
- Linearise z-coordinate equations about mean flow  $\overline{U}$  and stratification  $\frac{\partial b}{\partial z} = N^2$
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$$w = \widehat{w} e^{i(kx+mz-\omega t)}$$
  
 $-m^2 \left( (-i\omega + ik\overline{U} - \nu k^2)^2 + f^2 \right) - k^2 N^2 = 0$ 



$$m^{2} = \frac{k^{2}N^{2}}{\left(\left(\omega - k\overline{U} + i\nu k^{2}\right)^{2} - f^{2}\right)} = \frac{k^{2}N^{2}}{\left(\left(\omega - k\overline{U}\right)^{2} - f^{2} + 2i\nu k^{2}(\omega - k\overline{U})\right)}$$

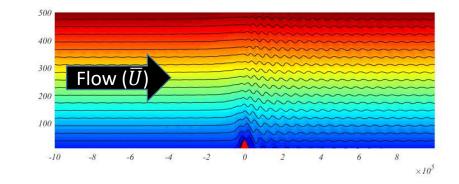


#### **Dispersion relation**

- Linearise z-coordinate equations about mean flow  $\overline{U}$  and stratification  $\frac{\partial b}{\partial z} = N^2$
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$$w = \widehat{w} e^{i(kx+mz-\omega t)}$$
  
 $-m^2 \left( (-i\omega + ik\overline{U} - \nu k^2)^2 + f^2 \right) - k^2 N^2 = 0$ 



 $\omega = k\overline{U} \pm \sqrt{f^2 + \frac{k^2 N^2}{m^2} - i \nu k^2}$  What is the effect of this? (Wave decays with time) Small dissipation approximation

$$m^{2} = \frac{k^{2}N^{2}}{\left((\omega - k\overline{U} + i\nu k^{2})^{2} - f^{2}\right)} = \frac{k^{2}N^{2}}{\left((\omega - k\overline{U})^{2} - f^{2} + 2i\nu k^{2}(\omega - k\overline{U})\right)} \simeq \frac{k^{2}N^{2}}{(\omega - k\overline{U})^{2} - f^{2}} \left(1 - \frac{2i\nu k^{2}(\omega - k\overline{U})}{(\omega - k\overline{U})^{2} - f^{2}}\right)$$

$$m \simeq \pm \frac{|k|N}{\sqrt{(\omega - k\overline{U})^2 - f^2}} \left(1 - \frac{i\nu k^2(\omega - k\overline{U})}{(\omega - k\overline{U})^2 - f^2}\right) = \pm m_0(1 - \gamma i) \qquad \text{Wave decays with depth}$$

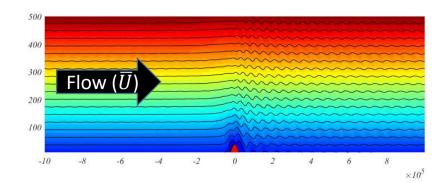
- Linearise z-coordinate equations about mean flow  $\overline{U}$  and stratification  $\frac{\partial b}{\partial z} = N^2$
- Assume no variation in y (ridge)

 $w = \widehat{w} \ e^{i(kx - m_0 z - \omega t) - \omega t}$ 

• Horizontal viscosity only = diffusivity

$$(D^{2} + f^{2})\frac{\partial^{2}w}{\partial z^{2}} + N^{2}\frac{\partial^{2}w}{\partial x} = 0 \qquad \text{Let} \quad w = \widehat{w} e^{i(kx+m\,z-\omega t)}$$
$$m \simeq -\frac{|k|N}{\sqrt{(\omega - k\overline{U})^{2} - f^{2}}} \left(1 - \frac{i\nu k^{2}(\omega - k\,\overline{U})}{(\omega - k\overline{U})^{2} - f^{2}}\right) = -m_{0}(1 - \gamma i)$$

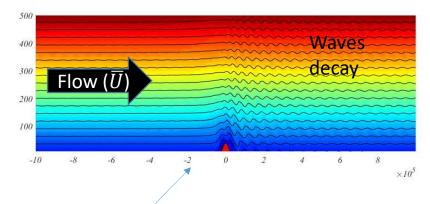
Wave decays as it propagates upwards



#### Lee wave solutions

- Linearise z-coordinate equations about mean flow  $\overline{U}$  and stratification  $\frac{\partial b}{\partial z} = N^2$
- Assume no variation in y (ridge)
- Horizontal viscosity only = diffusivity

$$(D^{2} + f^{2})\frac{\partial^{2}w}{\partial z^{2}} + N^{2}\frac{\partial^{2}w}{\partial x} = 0 \qquad \text{Let} \quad w = \widehat{w} e^{i(kx+m\,z-\omega t)}$$
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Solution plotted here

 $w = \widehat{w} e^{i(kx - 0^{z - \omega t}) - \omega t}$ 

Wave decays as it propagates upwards

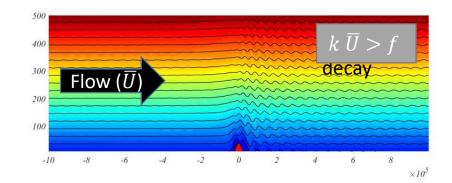
Let  $\underline{\omega} = \underline{0}$  and we need a boundary condition

$$w_0 = (u + \overline{U}) \frac{dh}{dx} \simeq \overline{U} \frac{dh}{dx} \to \widehat{w} = i \ k\overline{U} \ \hat{h}$$

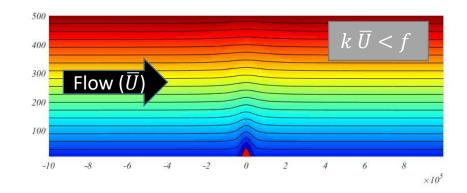
$$\rightarrow w = i \, k \overline{U} \, \widehat{h} \, e^{i(kx - m_0 z) - \gamma z}$$

#### Lee wave solutions

$$m_0 = \frac{|k|N}{\sqrt{(k\overline{U})^2 - f^2}} \qquad w = i \ k\overline{U} \ \hat{h} \ e^{i(kx - m_0 z) - \gamma z}$$

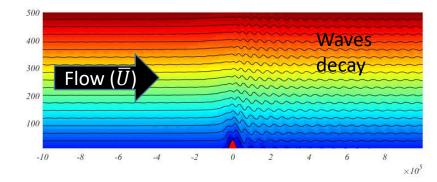


- The wavenumber is only real (waves exist) for  $k \ \overline{U} > f$
- This is what we mean by "fast enough"



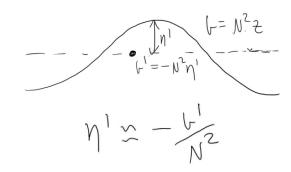
Solution for vertical

velocity: 
$$w = \int i \ k \overline{U} \ \hat{h} \ e^{i(kx - m_0 z) - \gamma z} \ dk = \int \hat{w} \ dk$$
  
Form stress:  $F = \int p \frac{\partial \eta'}{\partial x} \ dx$ 



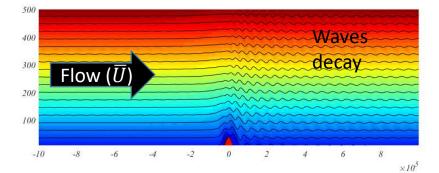
Equation tool kit:

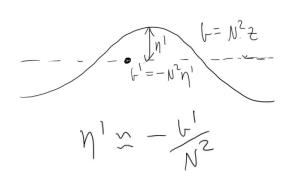
$$D u - fv = -\frac{1}{\rho_0} \frac{\partial p}{\partial x}$$
$$Dv + fu = 0$$
$$b = \frac{1}{\rho_0} \frac{\partial p}{\partial z}$$
$$\frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} = 0$$
$$Db + N^2 w = 0$$
$$D \simeq \overline{U} \frac{\partial}{\partial x}$$

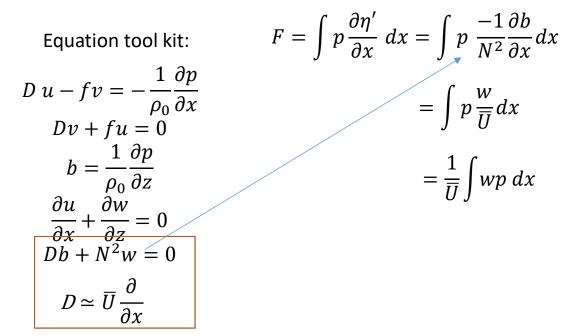


Solution for vertical velocity:

velocity: 
$$w = \int i \, k \overline{U} \, \hat{h} \, e^{i(kx - m_0 z) - \gamma z} \, dk = \int \hat{w} \, dk$$
  
Form stress:  $F = \int p \frac{\partial \eta'}{\partial x} \, dx$ 





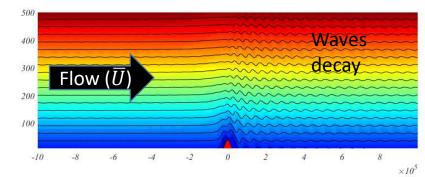


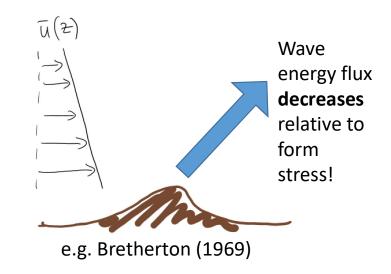
Solution for vertical velocity:

velocity: 
$$w = \int i \, k \overline{U} \, \hat{h} \, e^{i(kx - m_0 z) - \gamma z} \, dk = \int \hat{w} \, dk$$
  
Form stress:  $F = \int p \frac{\partial \eta'}{\partial x} \, dx$ 

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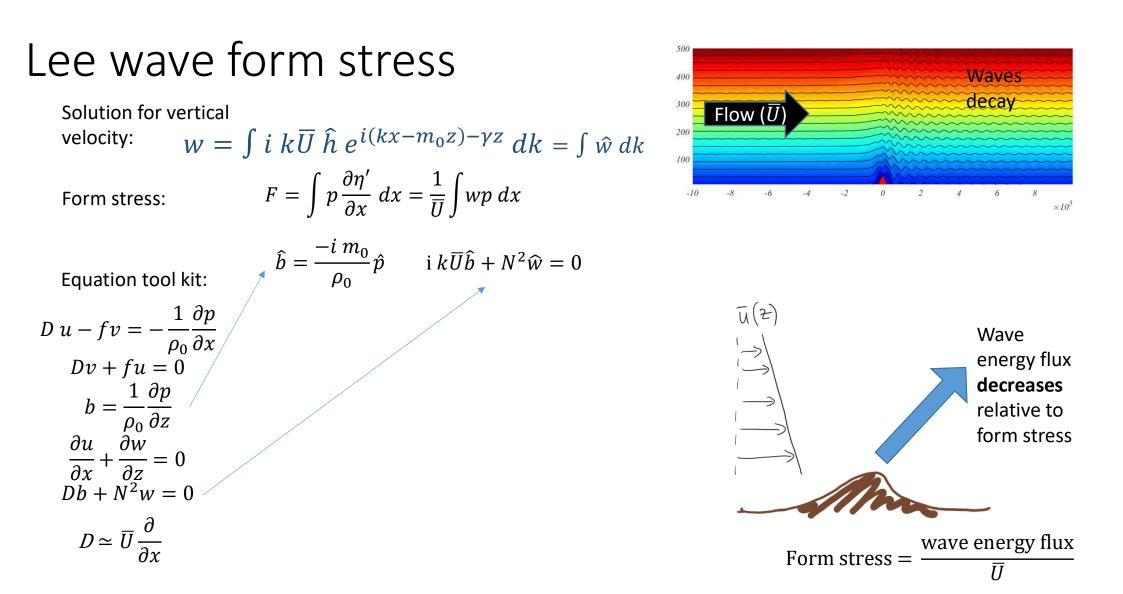
Equation tool kit:  $D u - fv = -\frac{1}{\rho_0} \frac{\partial p}{\partial x}$ Dv + fu = 0 $b = \frac{1}{\rho_0} \frac{\partial p}{\partial z}$  $\partial u \quad \partial w$ = 0 $Db + N^2w = 0$  $D \simeq \overline{U} \frac{\partial}{\partial r}$ 

$$F = \int p \frac{\partial \eta}{\partial x} dx = \int p \frac{-1}{N^2} \frac{\partial b}{\partial x} dx$$
$$= \int p \frac{w}{\overline{U}} dx$$
$$= \frac{1}{\overline{U}} \int wp dx$$

r

1 26

Form stress = 
$$\frac{\text{wave energy flux}}{\overline{U}}$$



#### Lee wave form stress 500 400 300 Solution for vertical Flow (U $w = \int i \, k \overline{U} \, \hat{h} \, e^{i(kx - m_0 z) - \gamma z} \, dk = \int \hat{w} \, dk$ 200 velocity: 100 $F = \int p \frac{\partial \eta'}{\partial x} \, dx = \frac{1}{\overline{U}} \int wp \, dx = \frac{1}{2\pi \overline{U}} \int \widehat{w} \, \widehat{p}^* \, dk$ Form stress: -10 -2 $\hat{b} = \frac{-i m_0}{2} \hat{p} \qquad i k \overline{U} \hat{b} + N^2 \hat{w} = 0$ Equation tool kit: $\hat{p} = -\rho_0 \frac{N^2}{m_0 k \overline{U}} \widehat{w}$ ū(2) $D u - fv = -\frac{1}{\rho_0} \frac{\partial p}{\partial x}$ Dv + fu = 0 $\widehat{\boldsymbol{w}}\,\,\widehat{\boldsymbol{p}}^* = -\rho_0 \frac{N^2}{m_0 k \overline{U}} \,|\widehat{\boldsymbol{w}}|^2$ $b = \frac{1}{\rho_0} \frac{\partial p}{\partial z}$ $\frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} = 0$ $Db + N^2 w = 0$ $D \simeq \overline{U} \frac{\partial}{\partial x}$ Form stress = -

Waves

decay

Wave

wave energy flux

 $\overline{II}$ 

energy flux

decreases

relative to form stress

×10<sup>4</sup>

0

2

#### Lee wave form stress 500 Waves 400 decay 300 Solution for vertical Flow (U $w = \int i \, k \overline{U} \, \hat{h} \, e^{i(kx - m_0 z) - \gamma z} \, dk = \int \hat{w} \, dk$ 200 velocity: 100 $F = \int p \frac{\partial \eta'}{\partial x} \, dx = \frac{1}{\overline{II}} \int wp \, dx = \frac{1}{2\pi \overline{II}} \int \widehat{w} \, \widehat{p}^* \, dk$ Form stress: -10 -2 0 2 $\hat{b} = \frac{-i m_0}{2} \hat{p} \qquad i k \overline{U} \hat{b} + N^2 \hat{w} = 0$ Equation tool kit: $\hat{p} = -\rho_0 \frac{N^2}{m_0 k \overline{U}} \widehat{w}$ ū(2) $D u - fv = -\frac{1}{\rho_0} \frac{\partial p}{\partial x}$ Wave energy flux Dv + fu = 0 $\widehat{\boldsymbol{w}}\,\widehat{\boldsymbol{p}}^* = -\rho_0 \frac{N^2}{m_0 k \overline{U}} \,|\widehat{\boldsymbol{w}}|^2$ decreases $b = \frac{1}{\rho_0} \frac{\partial p}{\partial z}$ relative to Energy flux = $\frac{-\rho_0 N^2}{m_0} \overline{U} |k| |\hat{h}|^2 e^{-2\gamma z}$ form stress $\frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} = 0$ $Db + N^2w = 0$ $D \simeq \overline{U} \frac{\partial}{\partial x}$ wave energy flux Form stress = - $\overline{II}$

 $\times 10^4$ 

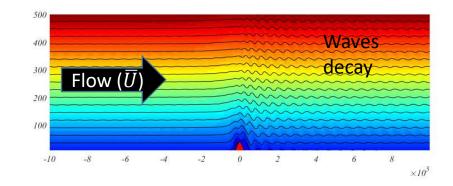
Energy flux = 
$$\frac{-\rho_0 N^2}{m_0} \overline{U} |k| |\hat{h}|^2 e^{-2\gamma z}$$

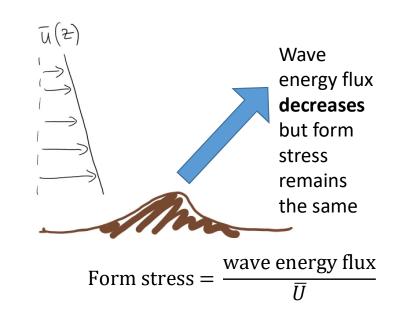
Form stress =  $\frac{-\rho_0 N^2}{m_0} |k| |\hat{h}|^2 e^{-2\gamma z}$ 

- Energy flux decays due to dissipation γ>0 and due to changes in mean flow (mean-to-wave exchanges)
- Form stress only decays due to dissipation  $\gamma>0$

#### **Conclusions:**

- A wave can lose (or gain) energy to a mean flow without changing its total form stress
  - Waves **do not** possess momentum e.g. McIntyre, 1981: "On the wave momentum myth"
- Form stress only decays (= force on the mean flow) if there is dissipation!
  - "non-acceleration theorem" e.g. Andrews and McIntyre (1978)





• Previously we came up with the mean momentum equation:

$$\frac{\partial u}{\partial t} + \underline{u} \cdot \nabla u + \underline{u}' \cdot \nabla u' - f \overline{v} = -\frac{1}{g_0} \frac{\partial \overline{p}}{\partial x} + v \nabla^2 \overline{u}$$
wave term.

• Rearranging we have that

$$\int_{T} \overline{u} - f \overline{v} = -\frac{1}{g_0} \frac{\partial \overline{p}}{\partial x} + v \overline{v}^2 \overline{u} - \nabla \cdot \left( \underline{u}' \underline{u}' \right)$$
 Rev

Reynolds stresses

- In the vertical direction this is  $\overline{u'w'}$  = vertical 'momentum flux'
- Are we done? Does this equal the stress from the hill?

Does 
$$-p' \frac{d\eta'}{dx} = \rho_0 u'w'$$
?  
Form stress Reynolds stress

$$\begin{aligned} \text{Does} &-p' \frac{d\eta'}{dx} = \rho_0 u'w'?\\ \text{Form stress} & \text{Reynolds stress} \end{aligned} \\ &-\int \rho' \frac{\partial h'}{\partial \chi} d\chi = + \int \frac{\partial \rho'}{\partial \chi} \eta' d\chi \quad \text{Integrate by parts} \end{aligned} \\ &= + \int \rho_0 \int \frac{Du'}{Dt} \eta' - f v' \eta' d\chi \quad \frac{\partial p'}{\partial \chi} = -\rho_0 \left(\frac{Du'}{Dt} - f v'\right) \end{aligned} \\ &= + \int \rho_0 \int \frac{D}{Dt} (u'\eta') - u' \frac{D\eta'}{Dt} - f v' \eta' d\chi \quad w' = \frac{D\eta'}{Dt} \end{aligned} \\ &= + \int \rho_0 \int \frac{D}{Dt} (u'\eta') - u' \frac{D\eta'}{Dt} - f v' \eta' d\chi \quad w' = \frac{D\eta'}{Dt} \end{aligned}$$

## The impact of waves (time varying flow) on the mean flow $\frac{1}{S_{0}}P'\frac{\partial n'}{\partial x} = u'w' + fv'\eta' - \frac{D}{Dt}(u'\eta')$ Stress on an isopycnal $\frac{1}{S_{0}}P'\frac{\partial n'}{\partial x} = u'w' + fv'\eta' - \frac{D}{Dt}(u'\eta')$

Can we re-write our previous momentum balance in terms of the isopycnal stress?

Momentum balance with stress at fixed z

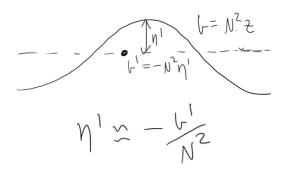
$$\overline{D}_{\overline{V}}\overline{u} - f\overline{v} = -\frac{1}{30}\overline{\partial x} + v\overline{v}\overline{u} - \nabla \cdot (\underline{u}'u')$$

Momentum balance with stress at fixed isopycnal (form stress)

$$\frac{D}{Dt} - f \overline{v}^* = -\frac{1}{3_0} \frac{\partial \overline{P}}{\partial z} + v \nabla^2 \overline{u} - \nabla \cdot \overline{E}$$

$$\frac{E}{E} = \left(\overline{u'u'}, \overline{u'v'}, \frac{1}{5_0} \overline{P'} \frac{\partial \eta'}{\partial z}\right)$$
Form stress
$$\overline{u^*} = \overline{u} + \frac{\partial}{\partial \overline{z}} \overline{u'\eta'}$$

$$\overline{v^*} = \overline{v} + \frac{\partial}{\partial \overline{z}} \overline{v'\eta'}$$



### The impact of waves (time varying flow) on the mean flow $\frac{1}{S_{b}} p^{i} \frac{\partial n^{i}}{\partial z} = u^{i} u^{i} + f v^{i} \eta^{i} - \frac{D}{Dt} (u^{i} \eta^{i})$

 $\eta' \simeq - b'_2$ 

Momentum balance with stress at fixed z

$$\overline{D}_{\overline{U}}\overline{u} - f\overline{v} = -\frac{1}{30}\overline{\partial r} + v\overline{\nabla^2 u} - \nabla \cdot (\underline{u}'u')$$

Momentum balance with stress at fixed isopycnal (form stress)

$$\frac{D\overline{u}}{Dt} - f\overline{v}^* = -\frac{1}{P_0} \underbrace{\partial \overline{p}}{\partial x} + v\nabla^2 \overline{u} - \nabla \circ \underbrace{Fep}$$

$$\underbrace{F_{Ep}} = \left(\overline{u'u'}, \overline{u'v'}, \overline{u'v'} - \frac{\overline{v'b'}}{N^2}\right) \underbrace{\text{Eliassen-Palm (EP)}}_{\text{Flux}}$$
Residual Flow
$$\overline{u^*} = \overline{u} + \underbrace{\partial \overline{z}}_{\overline{v}\overline{v}} \underbrace{u'\eta'}_{\overline{v}\overline{v}} = \overline{u} - \frac{\overline{u'b'}}{N^2}$$

$$\overline{v^*} = \overline{v} + \underbrace{\partial \overline{z}}_{\overline{v}\overline{v}\overline{v}\overline{v}} = \overline{v} - \frac{\overline{v'b'}}{N^2}$$

You get the same result by integrating from the bottom to some isopycnal (as you might do when calculating the MOC in density space....)

$$\int_{h}^{h_{1}} \frac{Du}{Dt} - fv = -\frac{1}{S_{b}} \frac{\partial P}{\partial x} + V \nabla^{2} u dv$$

$$= -\frac{1}{S_{b}} \int_{h}^{h} \frac{\partial P}{\partial x} dz \quad * \text{It must be true that } \frac{D\eta}{Dt} = 0 \text{ for this step}$$

$$= -\frac{1}{S_{b}} \int_{h}^{h} \frac{\partial P}{\partial x} dz - \frac{1}{S_{b}} \int_{h}^{h+h} \frac{\partial P}{\partial x} dz \quad \text{Split the mean and wave parts}$$

$$= -\frac{1}{S_{b}} \int_{h}^{h} \frac{\partial P}{\partial x} dz - n \quad \frac{\partial P}{\partial x}$$

$$= -\frac{1}{S_{b}} \int_{h}^{h} \frac{\partial P}{\partial x} dz - n \quad \frac{\partial P}{\partial x}$$
Make the small amplitude approximation
$$\frac{D}{Dt} \left( \frac{\partial}{\partial N} \int_{h}^{h} u dz \right) - \frac{1}{S_{b}} \int_{h}^{h} u dz = -\frac{1}{S_{b}} \frac{\partial P}{\partial x} - \frac{\partial}{\partial N} \left( \gamma \quad \frac{\partial P}{\partial x} \right)$$
Take the gradient with respect to mean isopycnal heights
Flow integrated from bottom to height
Form stress

#### What does this all mean?

Suppose we have a steady mean flow, with small Rossby number (neglect advection)

$$\frac{D\overline{u}}{Dt} - f\overline{v}^* = -\frac{1}{P_0} \frac{\partial\overline{p}}{\partial x} + v\overline{v}^2\overline{u} - \nabla \cdot \overline{F_{EP}}$$

$$\overline{F_{EP}} = (\overline{u'u'}, \overline{u'v'}, \overline{u'w' - \frac{v'b'}{N^2}})$$

Take a zonal average (denote by []) and assume the domain is periodic (e.g. the ACC)

$$-f\left[\overline{v}^{*}\right] = -\frac{\partial}{\partial y}\left[\overline{u^{\prime}u^{\prime}}\right] - \frac{\partial}{\partial z}\left[\overline{u^{\prime}w^{\prime}} - \frac{v^{\prime}b^{\prime}}{N^{2}}\right] + \sqrt{\frac{\partial^{2}\overline{u}}{\partial y^{2}}} + \sqrt{\frac{\partial^{2}\overline{u}}{\partial z^{2}}}$$

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$$\frac{D\overline{u}}{Dt} - f\overline{v}^* = -\frac{1}{P_0} \frac{\partial\overline{p}}{\partial x} + v\overline{v}^2\overline{u} - \nabla \cdot \underline{F}_{EP}$$

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Take a zonal average (denote by []) and assume the domain is periodic (e.g. the ACC)

$$-f\left[\overline{v}^*\right] = -\frac{\partial}{\partial g}\left[\overline{u^{\dagger}u^{\dagger}}\right] - \frac{\partial}{\partial z}\left[\overline{u^{\dagger}u^{\dagger}} - \frac{v^{\dagger}b^{\dagger}}{N^{2}}\right] + \sqrt{\frac{\partial^{2}u}{\partial z^{2}}} + \sqrt{\frac{\partial^{2}u}{\partial z^{2}}}$$

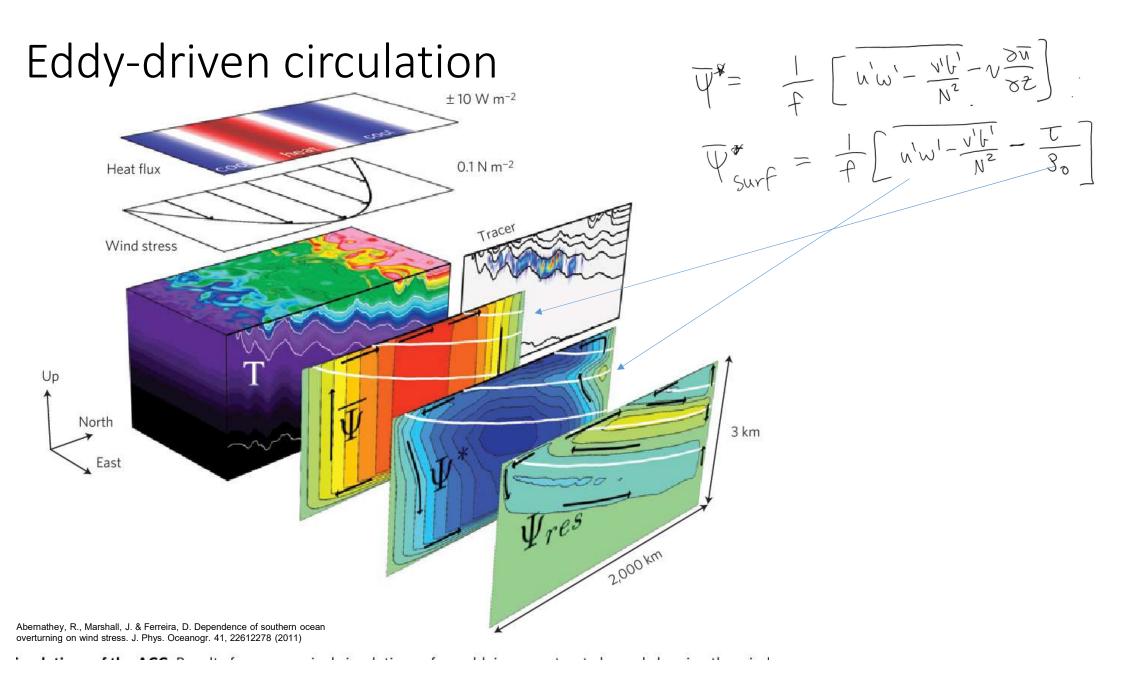
$$\overline{v}^* = \frac{\partial\overline{v}^*}{\partial \overline{z}} \qquad \overline{v}^* = \frac{1}{F}\left[\overline{u^{\dagger}u^{\dagger}} - \frac{v^{\dagger}b^{\dagger}}{N^{2}} - \sqrt{\frac{\partial\overline{u}}{\partial \overline{z}}}\right] \quad \text{"Residual" streamfunction}$$

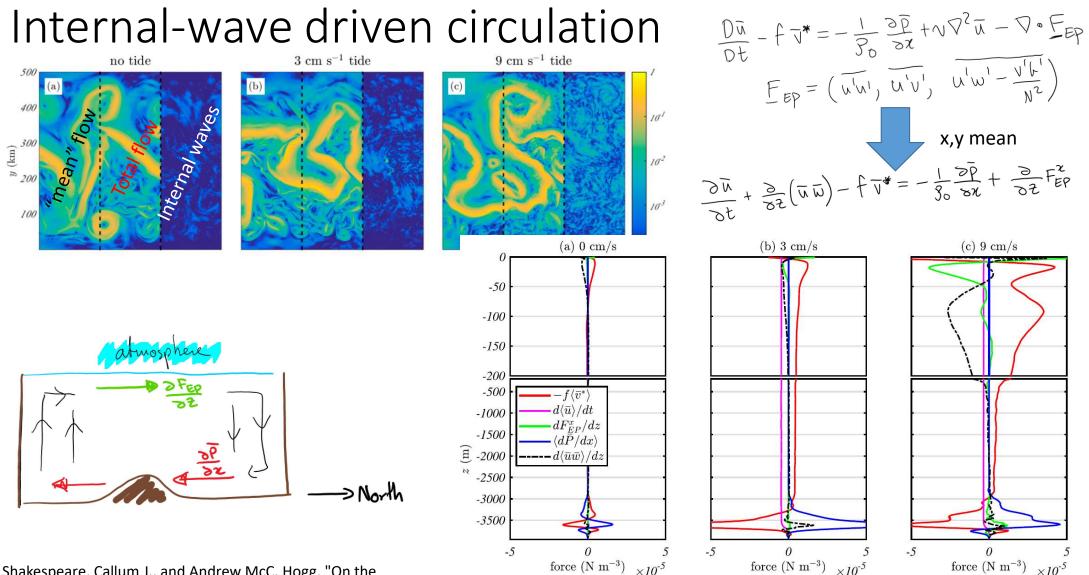
$$\overline{v}^* = \frac{1}{F}\left[\overline{u^{\dagger}u^{\dagger}} - \frac{v^{\dagger}b^{\dagger}}{N^{2}} - \frac{\overline{v}}{3\sigma}\right] \quad \text{Value at surface}$$

$$\text{Wave (or}$$

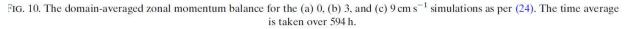
$$\text{eddy) driven}$$

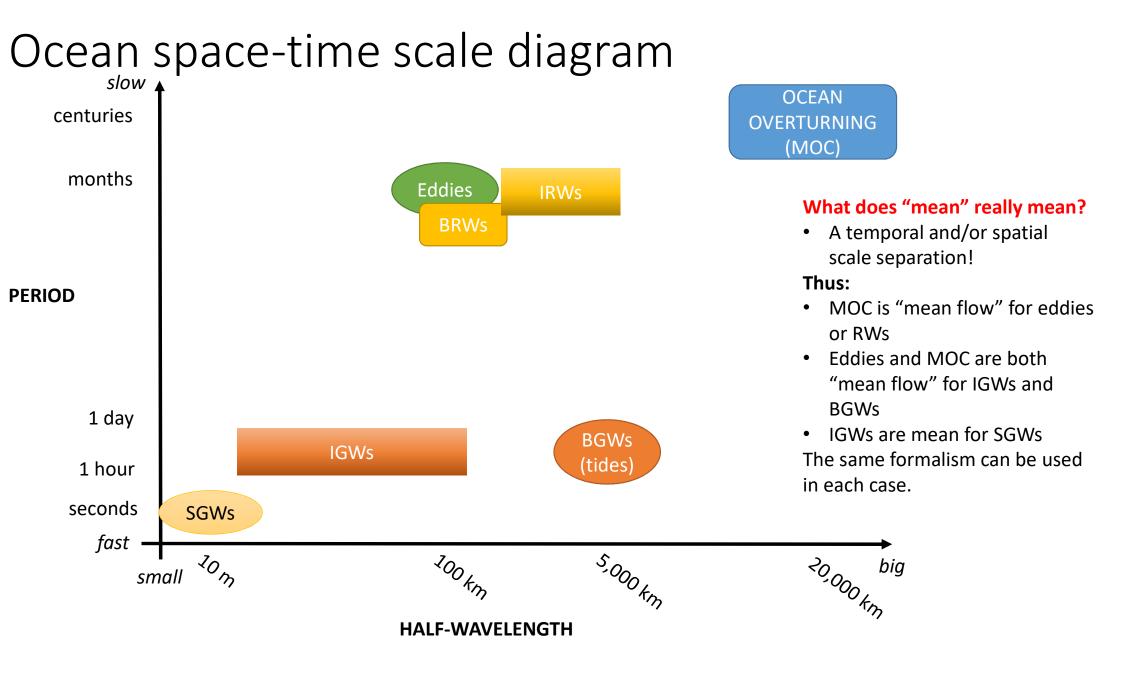
$$\text{circulation}$$





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